

DIFUSIVIDAD EN GASES.

a) Ecuación de Chapman-Enskog

$$D_{AB} [\text{cm}^2/\text{s}] = \frac{0.001858 \cdot T^{3/2} \cdot \left[\frac{M_A + M_B}{M_A \cdot M_B} \right]^{1/2}}{P \cdot \sigma_{AB}^2 \cdot \Omega_D}$$

T[K] P[atm] M:[g/mol]

b) Correlación empírica de Slattery y Bird

$$D_{AB} [\text{cm}^2/\text{s}] = \left(\frac{2.74 \cdot 10^{-4}}{P} \right) \cdot \left(\frac{M_A + M_B}{M_A \cdot M_B} \right)^{1/2} (P_{C_A} P_{C_B})^{1/3} (T_{C_A} T_{C_B})^{-0.495} T^{1.823}$$

DIFUSIVIDAD EN SOLUCIONES

a) Correlación de Wilke-Chang

$$D_{AB} [\text{cm}^2 / \text{s}] = 7.4 \cdot 10^{-8} \left[\frac{(\Phi \cdot M_B)^{1/2} \cdot T}{\mu_B \cdot V_A^{0.6}} \right]$$

M [g/mol] T[K] μ_B [cp] V_A : V molar del soluto en el pto. normal de ebullición[cm³/mol]

Φ : parámetro de asociación del solvente (2.6 para el H₂O) A:soluto B:solvente

b) Correlación de Sheibel

$$D_{AB} [\text{cm}^2 / \text{s}] = \frac{K \cdot T}{\mu_B \cdot V_A^{0.6}} \quad K = 8.2 \cdot 10^{-8} \left[1 + \left(\frac{3 \cdot V_B}{V_A} \right)^{2/3} \right]$$

Ref.: idem anterior

DIFUSIVIDAD EN SÓLIDOS

Difusividad Knudsen

$$D_K [\text{cm}^2 / \text{s}] = 9.7 \cdot 10^3 \bar{r}_p [\text{cm}] \sqrt{\frac{T[\text{K}]}{M \cdot [\text{g/mol}]}}$$

$$D_{\text{combinada}} = \frac{1}{\frac{1}{D_K} + \frac{1}{D_{AB}}}$$

$$D_{\text{efectiva}} = D_{\text{combinada}} \frac{\varepsilon}{\tau}$$

LAS ECUACIONES DE VARIACIÓN

18-5

TABLA 18.2-1
 LA ECUACIÓN DE CONTINUIDAD DE A EN DIVERSOS SISTEMAS
 COORDENADOS
 (Ec. 18.1-10)

Coordenadas rectangulares:

$$\frac{\partial c_A}{\partial t} + \left(\frac{\partial N_{Ax}}{\partial x} + \frac{\partial N_{Ay}}{\partial y} + \frac{\partial N_{Az}}{\partial z} \right) = R_A \quad (A)$$

Coordenadas cilíndricas:

$$\frac{\partial c_A}{\partial t} + \left(\frac{1}{r} \frac{\partial}{\partial r} (r N_{Ar}) + \frac{1}{r} \frac{\partial N_{A\theta}}{\partial \theta} + \frac{\partial N_{Az}}{\partial z} \right) = R_A \quad (B)$$

Coordenadas esféricas:

$$\frac{\partial c_A}{\partial t} + \left(\frac{1}{r^2} \frac{\partial}{\partial r} (r^2 N_{Ar}) + \frac{1}{r \sin \theta} \frac{\partial}{\partial \theta} (N_{A\theta} \sin \theta) + \frac{1}{r \sin \theta} \frac{\partial N_{A\phi}}{\partial \phi} \right) = R_A \quad (C)$$

TABLA 18.2-2
 LA ECUACIÓN DE CONTINUIDAD DE A PARA ρ Y \mathcal{D}_{AB} CONSTANTES
 (Ec. 18.1-17)

Coordenadas rectangulares:

$$\frac{\partial c_A}{\partial t} + \left(v_x \frac{\partial c_A}{\partial x} + v_y \frac{\partial c_A}{\partial y} + v_z \frac{\partial c_A}{\partial z} \right) = \mathcal{D}_{AB} \left(\frac{\partial^2 c_A}{\partial x^2} + \frac{\partial^2 c_A}{\partial y^2} + \frac{\partial^2 c_A}{\partial z^2} \right) + R_A \quad (A)$$

Coordenadas cilíndricas:

$$\begin{aligned} \frac{\partial c_A}{\partial t} + \left(v_r \frac{\partial c_A}{\partial r} + v_\theta \frac{1}{r} \frac{\partial c_A}{\partial \theta} + v_z \frac{\partial c_A}{\partial z} \right) \\ = \mathcal{D}_{AB} \left(\frac{1}{r} \frac{\partial}{\partial r} \left(r \frac{\partial c_A}{\partial r} \right) + \frac{1}{r^2} \frac{\partial^2 c_A}{\partial \theta^2} + \frac{\partial^2 c_A}{\partial z^2} \right) + R_A \end{aligned} \quad (B)$$

Coordenadas esféricas:

$$\begin{aligned} \frac{\partial c_A}{\partial t} + \left(v_r \frac{\partial c_A}{\partial r} + v_\theta \frac{1}{r} \frac{\partial c_A}{\partial \theta} + v_\phi \frac{1}{r \sin \theta} \frac{\partial c_A}{\partial \phi} \right) \\ = \mathcal{D}_{AB} \left(\frac{1}{r^2} \frac{\partial}{\partial r} \left(r^2 \frac{\partial c_A}{\partial r} \right) + \frac{1}{r^2 \sin \theta} \frac{\partial}{\partial \theta} \left(\sin \theta \frac{\partial c_A}{\partial \theta} \right) + \frac{1}{r^2 \sin^2 \theta} \frac{\partial^2 c_A}{\partial \phi^2} \right) + R_A \end{aligned} \quad (C)$$

ANALOGÍAS ENTRE TRANSMISIÓN DE CALOR Y MATERIA
 A BAJAS VELOCIDADES DE TRANSFERENCIA DE MATERIA

	Magnitudes de transmisión de calor	Magnitudes de transferencia binaria de materia
Perfiles	T	x_A
Difusividad	$\alpha = \frac{k}{\rho \hat{C}_p}$	\mathcal{D}_{AB}
Efecto de los perfiles sobre la densidad	$\beta = -\frac{1}{\rho} \left(\frac{\partial \rho}{\partial T} \right)_{p, x_A}$	$\zeta = -\frac{1}{\rho} \left(\frac{\partial \rho}{\partial x_A} \right)_{p, T}$
Densidad de flujo	$q^{(c)}$	$J_A^* = N_A - x_A(N_A + N_B)$
Velocidad de transferencia	Q	$h_A^{(m)} - x_{A0}(h_A^{(m)} + h_B^{(m)})$
Coefficiente de transferencia	$h = \frac{Q}{A \Delta T}$	$k_x = \frac{h_A^{(m)} - x_{A0}(h_A^{(m)} + h_B^{(m)})}{A \Delta x_A}$
Grupos adimensionales que son iguales en ambas correlaciones	$Re = \frac{DV\rho}{\mu} = \frac{DG}{\mu}$	$Re = \frac{DV\rho}{\mu} = \frac{DG}{\mu}$
	$Fr = \frac{V^2}{gD}$	$Fr = \frac{V^2}{gD}$
	$\frac{L}{D}$	$\frac{L}{D}$
Grupos adimensionales básicos que son diferentes en ambas correlaciones	$Nu = \frac{hD}{k}$	$Nu_{AB} = \frac{k_x D}{c \mathcal{D}_{AB}}$
	$Pr = \frac{\hat{C}_p \mu}{k} = \frac{\nu}{\alpha}$	$Sc = \frac{\mu}{\rho \mathcal{D}_{AB}} = \frac{\nu}{\mathcal{D}_{AB}}$
	$Gr = \frac{D^3 \rho^2 g \beta \Delta T}{\mu^2}$	$Gr_{AB} = \frac{D^3 \rho^2 g \zeta \Delta x_A}{\mu^2}$
	$St = \frac{Nu}{Re Pr} = \frac{h}{\rho \hat{C}_p V}$	$St_{AB} = \frac{Nu_{AB}}{Re Sc} = \frac{k_x}{c V}$
Combinaciones especiales de grupos adimensionales	$Pé = Re Pr = \frac{DV\rho \hat{C}_p}{k}$	$Pé_{AB} = Re Sc = \frac{DV}{\mathcal{D}_{AB}}$
	$j_H = Nu Re^{-1} Pr^{-1/4} = \frac{h}{\rho \hat{C}_p V} \left(\frac{\hat{C}_p \mu}{k} \right)^{3/4}$	$j_D = Nu_{AB} Re^{-1} Sc^{-1/4} = \frac{k_x}{c V} \left(\frac{\mu}{\rho \mathcal{D}_{AB}} \right)^{3/4}$

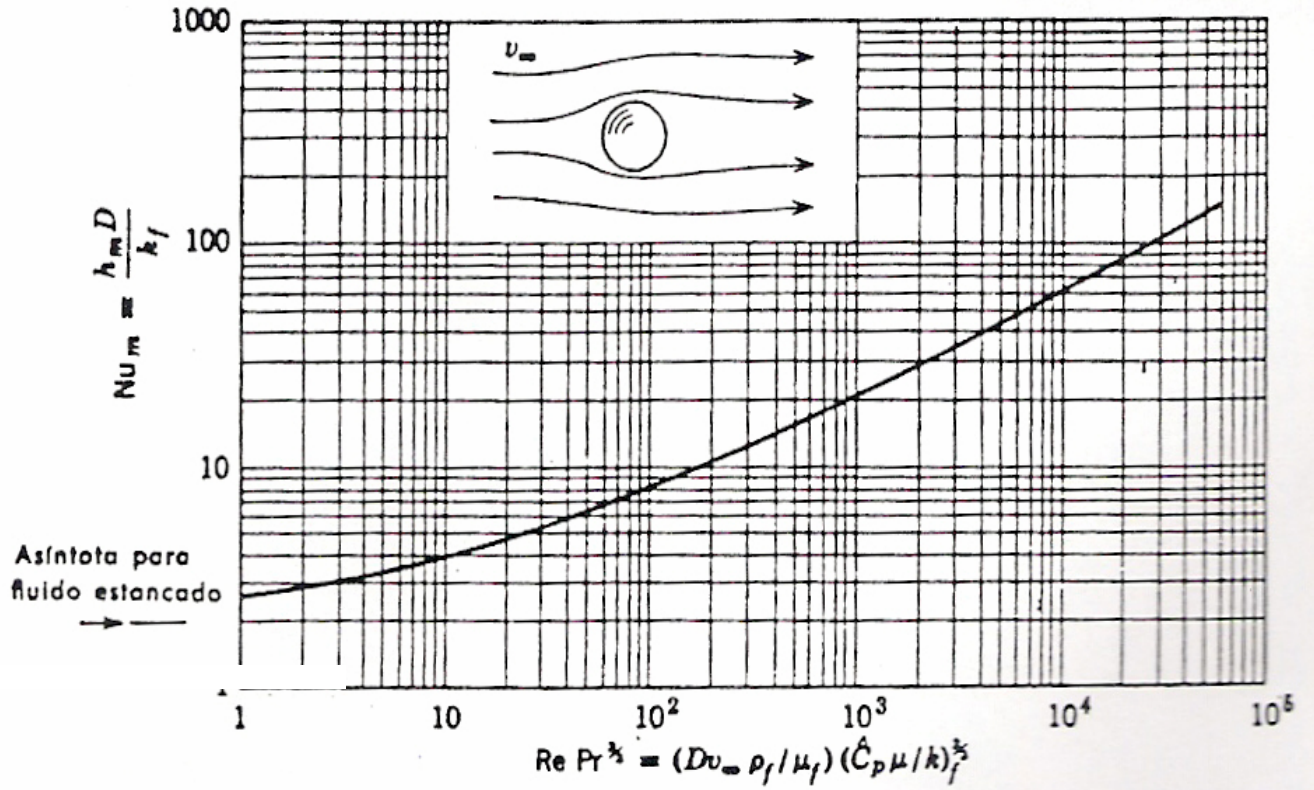


Fig. 13.3-2. Transmisión de calor por convección forzada desde una esfera aislada. [W. E. RANZ y W. R. MARSHALL, Jr, *Chem. Eng. Prog.*, 48, 141-146, 173-180 (1952).]

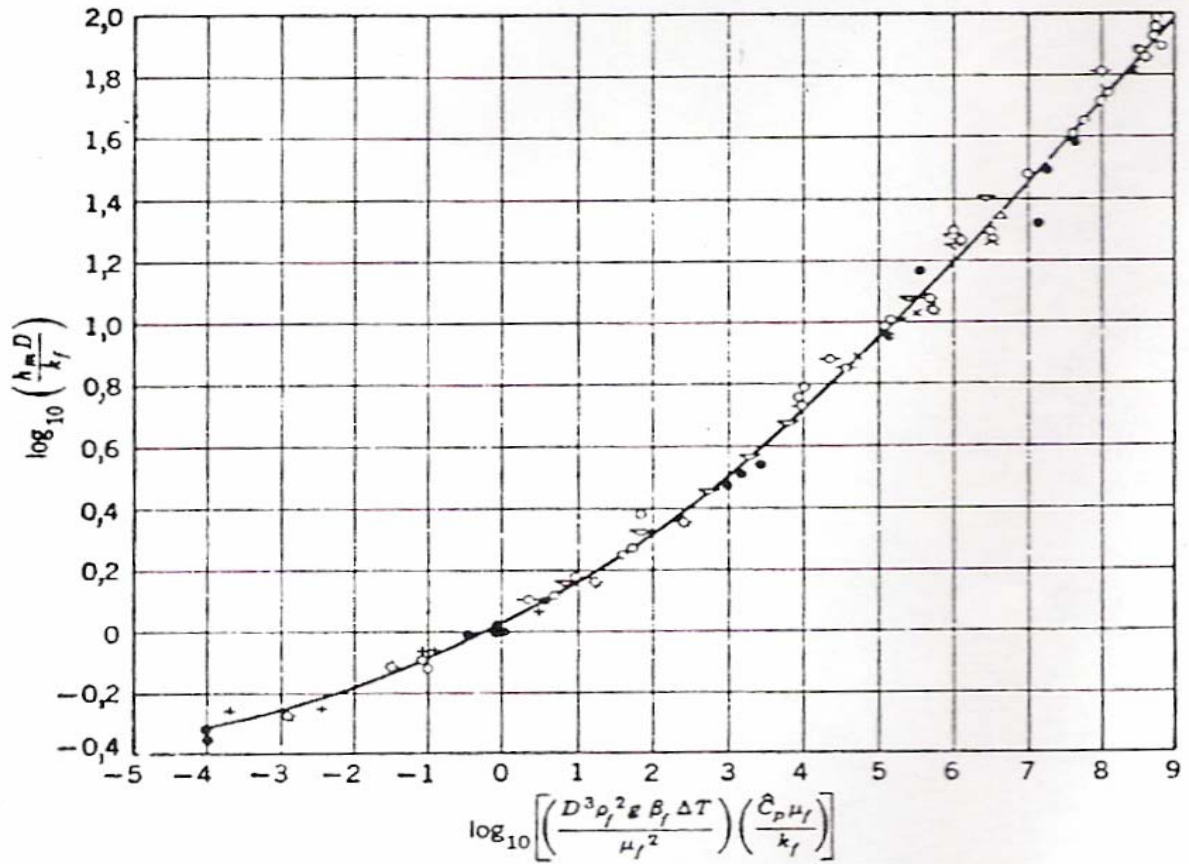


Fig. 13.5-1. Convección libre a diversos fluidos desde largos tubos horizontales. [W. H. MCADAMS, *Heat Transmission*, McGraw-Hill, Nueva York (1954), tercera edición, p. 176].

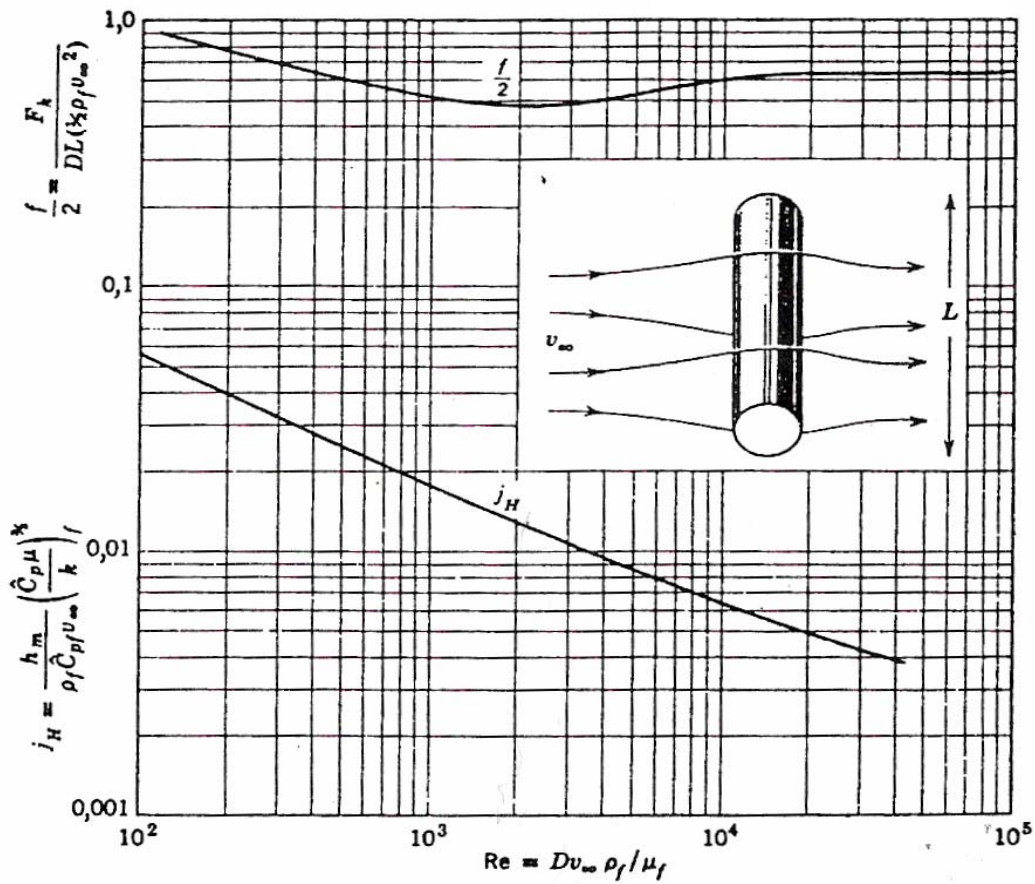


Fig. 13.3-1. Transferencia de calor y cantidad de movimiento entre un cilindro largo y una corriente transversal. [j_H está tomado de T. K. Sherwood y R. L. Pigford. *Absorption and Extraction*, McGraw-Hill, Nueva York (1952), segunda edición, p. 70; $f/2$ está tomado de H. Schlichting, *Boundary-Layer Theory*, Pergamon, Nueva York (1955), p. 16.]